



SPEAKERS



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PVcase Ground Mount PM



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CONTENTS

Nevados Project Development

- Project Development Workflow
- CAD Blocks Configurations
- TOPO Data
- Layout Optimization
- Constant Reveal Height

Terrain Following Layout w/ PVcase

- Tracker Configurations
- Standard Layout
- Layout Iterations



Why Nevados?

Our objective is to offer cost-effective solar tracking solutions that eliminate the need for site grading.



We design each site to be installed, including engineering and construction schedule, which not everybody does



We make dealing with specialized and complex sites simple

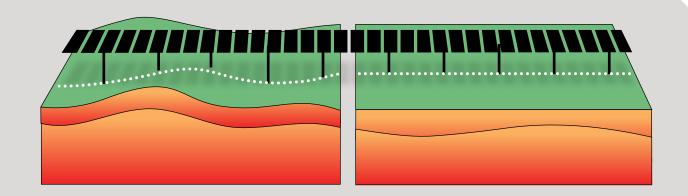


Because the world is not flat

Our Approach to Terrain

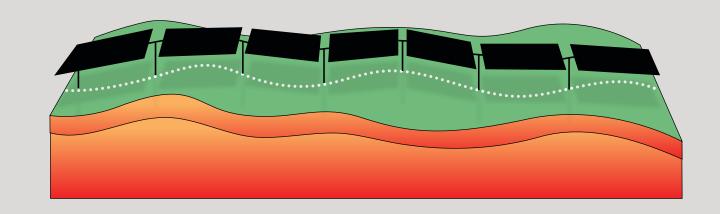
Traditional Tracker

Historically, Trackers deal with rolling terrain by variable foundation reveal height with a limited ability to handle slope change.



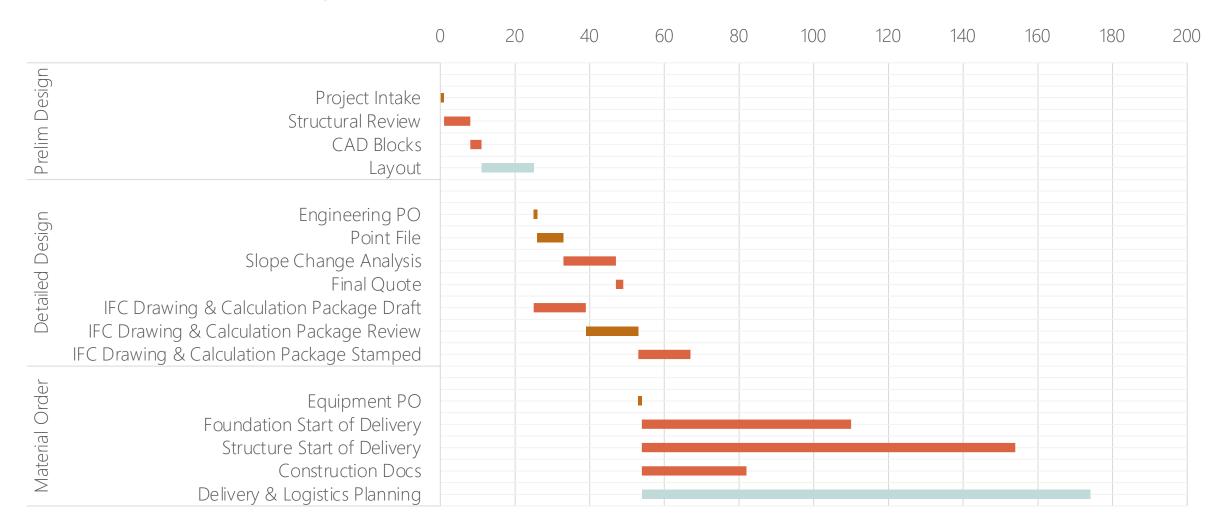
Nevados All Terrain Tracker (ATT)

Our tracker has consistent foundation reveal height regardless of the terrain, interchangeable proprietary bearings enable easy terrain following. Our ATT is capable of handling up to a 26% slope change across a foundation





NEVADOS PROJECT DESIGN/PROCUREMENT TIMELINES





NEVADOS WORK FLOW

Pre-Award <30%:

Task/Deliverable	Est. Time to Completion
Project data input collection	1 – 5 days pending customer response and information
Structural Review and TOPL Report	1 day
CAD Blocks	Same day as Structural
Preliminary Layout	1-7 days
B.O.M.	1 day
Full Proposal	3-7 days

Late Stage >30% with Engineering PO:

Task/Deliverable	Est. Time to Completion
Final Structural Review	1 Day
Final Layout	Pending customer
Point File	2 weeks
Final BOM	1 day
Preliminary 60% IFC Draft	1-2 weeks

Post Award:

Task/Deliverable	Est. Time to Completion
Equipment Layouts	30 days before 1st delivery
Stamped IFC with PE calcs	2 weeks





PROJECT DATA COLLECTION

- Minimum Requirements to start project proposal
 - Site location and coordinates
 - Target DC capacity
 - Module information and datasheet
 - String size
 - GCR
 - U.S. content for manufacturing
 - Site boundaries (AutoCAD and KMZ)
 - Foundations
 - Expected First Delivery

- Additional Information
 - ASCE Code
 - Risk Category
 - Snow Load
 - Wind Speed
 - Leading Edge
 - CAB Requirement (Row End/Motor/Other)
 - North South Row Spacing
 - Boundary offsets (Road, Fences, Wetlands, Etc.)
 - Geotech Reports
 - Pull-test Report
 - Preliminary Layout

Structural Review and **TOPL Reports**

- Nevados optimizes steel for every project and site
- Site conditions are critical to understand to generate functional reports
- TOPLs will need to be generated to design foundations

es:			

Fh - Horizontal force due to wind load Fy - Vertical force due to wind load

Fa - Axial load due to wind load

Ma - Moment at slew drive due to south and north wing

Ma-1A Moment due to Mechanical stop - north wing

Ma-2A Moment due to Mechanical stop - south wing

Ma-1B Moment due to Mechanical stop - north wing Ma-2B Moment due to Mechanical stop - south wing

Z = Distance between axis of rotation and top of the post.

Z1 - Distance to slew drive axis of rotation from top of the post.

Z2 - Distance to axis of rotation for non-drive and mechanical stop posts from top of the post Z3 - Distance to axis of rotation for row end and articulating posts from top of the post

77.00 lb

PE/SE team to sign above, Customer to confirm Module size

First Solar FS6 435W

79.09 in

48.50 in

1.91 in

Module Info:

Manufacturer

Chord Length (L)

Model

Width (W)

Weight (Wt)



Row Configuration:

84 Modules per Row

42 Modules per North Wing

Design Leading Edge Height

42 Modules per South Wing

Max Drive Post Reveal Height	65
Max Non-Drive Post Reveal Height	72
Design Drive Post Reveal Height	60
Design Non-Drive Post Reveal Heigh	67

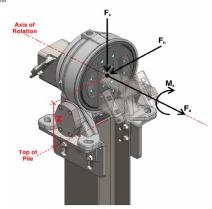


Figure - A, Direction of Loads

Design Parameters

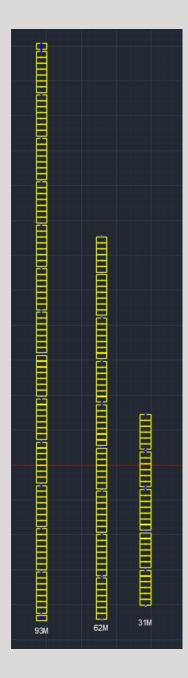
Max Wind Speed (per ASCE 7-16)	87	MPH
Operational Wind Speed (3-second gust)	42	MPH
Operational Wind Speed (10-second gust)	35	MPH
Snow Load	0	psf
Stow Angle	60	degrees
Snow Stow Angle	60	degrees
Exposure Class	C	
Max Slope	2.5	degrees
Seismic Load Sds*	1.014	g
Ground Elevation Factor, Ke	0.99	-

PE/SE team to sign above. Customer to confirm design/site parameters

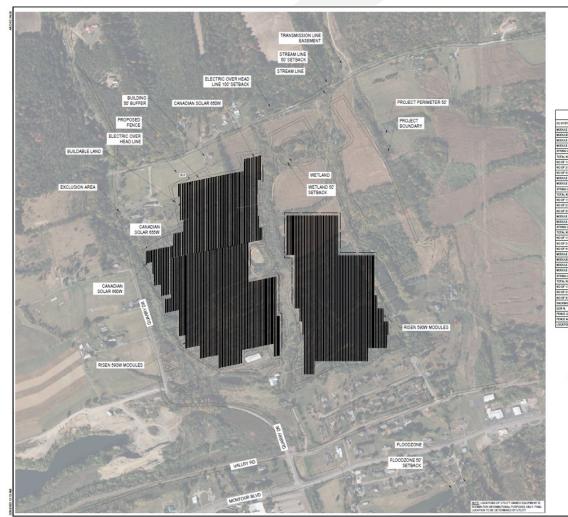
1 2 3	Perimeter Non-Drive Post Perimeter Non-Drive Post Perimeter Mechanical Stop Post	Load Case #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #5b, Max Seismic Load #5b, Max Seismic Load #5a, Max Wind Downforce #3, Max Wind Downforce #5b, Max Seismic Load #7b, Max Seismic Load #5b, Max Wind Downforce #3, Max Wind Downforce #5b, Max Seismic Load #5b, Max Seismic Load #5b, Max Seismic Load	0 0 -2209 2114 0 0 -2209	Fv (lbs) -848 -848 -826 -713 -712 -848 -2826 -713 -712 -848	19 31 31 261 19 31 261 261	-875 -1101 	Ma-1A (ft.lbs)	Ma-1B (ft.lbs)	Ma-1C (ft.lbs)	Ma-2A (ft.lbs)	Ma-2B (ft.lbs)	Ma-2C (ft.lb
	Perimeter Non-Drive Post Perimeter Non-Drive Post Perimeter Mechanical Stop Post	#5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Nimd Downforce #3, Max Seismic Load #5b, Max Seismic Load #5, Max Wind Downforce #3, Max Snow Load #5a, Max Snow Load	2114 0 0 -2209 2114 0 0 -2209	2826 713 712 -848 2826 713 712 -848	31 31 261 19 31 31	-1101		-		-	-	- :
	Perimeter Non-Drive Post Perimeter Non-Drive Post Perimeter Mechanical Stop Post	#3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	0 0 -2209 2114 0 0 -2209	713 712 -848 2826 713 712 -848	31 261 19 31 31			-		-	-	- :
	Perimeter Non-Drive Post Perimeter Mechanical Stop Post	#5b, Max Seismic Load #7, Max Wind Uptith #5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uptith #5a, Max Wind Downforce #3, Max Snow Load	0 -2209 2114 0 0 -2209	712 -848 2826 713 712 -848	261 19 31 31	-	- :	- :	- :	-	- :	
	Perimeter Non-Livive Post Perimeter Mechanical Stop Post	#7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	-2209 2114 0 0 -2209	-848 2826 713 712 -848	19 31 31	- :	- :	-	- 1	-	-	
	Perimeter Non-Livive Post Perimeter Mechanical Stop Post	#5a, Max Wind Downforce #3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	2114 0 0 -2209	2826 713 712 -848	31	-	- 1					
	Perimeter Non-Livive Post Perimeter Mechanical Stop Post	#3, Max Snow Load #5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	0 0 -2209	713 712 -848	31	_						
	Perimeter Mechanical Stop Post	#5b, Max Seismic Load #7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	-2209	712		-						
3	Penmeter Mechanical Stop Post	#7, Max Wind Uplift #5a, Max Wind Downforce #3, Max Snow Load	-2209	-848	261		-	-	-	-	-	-
3	Penmeter Mechanical Stop Post	#5a, Max Wind Downforce #3, Max Snow Load				-						
3	Penmeter Mechanical Stop Post	#3, Max Snow Load	2114		19	-	-1792	-1750	-1312	-1312	-1750	-1792
3	450000000000000000000000000000000000000			2826	31	-	-2243	-2201	-1651	-1651	-2201	-2243
		#5h May Seismir Load	0	713	31	2.	-	/	- 2	-	-	-
			0	712	261	-				-	-	-
		#7. Max Wind Uplift	-1105	-424	19	-		-	-			-
		#5a. Max Wind Downforce	1057	1413	31	-		1-0			-	-
4	4 Perimeter Row-End Non-Drive Post	#3. Max Snow Load	0	356	31							
		#5b. Max Seismic Load	0	356	261							
		#7, Max Wind Uplift	-1150	-238	19	-1998		-				
	0.0000000000000000000000000000000000000	#5a, Max Wind Downforce	1393	2106	31	-406						
5	Interior Drive Post	#3. Max Snow Load		713	31			-				
		#5b. Max Seismic Load		712	261							
		#7. Max Wind Uplift		-236	19		-			-	-	
23		#5a. Max Wind Downforce	1393	2106	31			-				
6	Interior Non-Drive Post	#3. Max Snow Load		713	31							
		#5b Max Seismic Load	0	712	261							
		#7. Max Wind Uplift		-236	19		-1374	0	-1665	-1665	0	-1374
1000		#5a, Max Wind Downforce		2106	31		-299	0	-321	-342	0	-299
7	Interior Mechanical Stop Post	#3 Max Snow Load		713	31			-			-	
		#5b. Max Seismic Load		712	261	-	-					-
		#7, Max Wind Uplift		-118	19					-		
		#5a, Max Wind Downforce	697	1053	31	-		-	-	-	-	-
8	8 Interior Row-End Non-Drive Post	#3. Max Snow Load		356	31		-	-			-	-
		#5b. Max Seismic Load	0	356	261	-	- :	-				-
		#7. Max Wind Uplift		-755	19		-		-	-		
		#5a. Max Wind Downforce		1632	31		-	-			-	-
9	Corner Row-End Non-Drive Post	#3. Max Snow Load		356	31	-	-	-	- 1		-	
		#5b. Max Seismic Load		356	261		-	-	- :	-		-

CAD Blocks & Preliminary Layouts (1 Week)

- Structural reviews will provide CAD block configurations
- To minimize reworking layouts, CAB requirements should be determined as early as possible
- A CAD of site boundaries will be required to build the most accurate layout
 - Roads, wetlands, offsets, etc.
 - Inverter size callouts
- GCR requirements or range



- Nevados ATT can open buildable areas
- Iterate layout with the customer
- Topo surface to identity potential areas for grading/non-grading
- 1 foot contour line is preferred
- Preliminary point file based off layout from customer, if possible, to generate the most accurate B.O.M.





Nevados Engineering, Inc.

Avados Engineering, Inc.
390 Termine ID, Ilia 698
Ilian Avados (A HIST
Term (A HIST)



PRELIMINARY NOT FOR CONSTRUCTION

PROPOSED ARRAY CONFIGURATION

E101

B.O.M. AND PROPOSAL

- B.O.M. are generated from preliminary layout
- Preliminary foundations can be included in the pricing if required



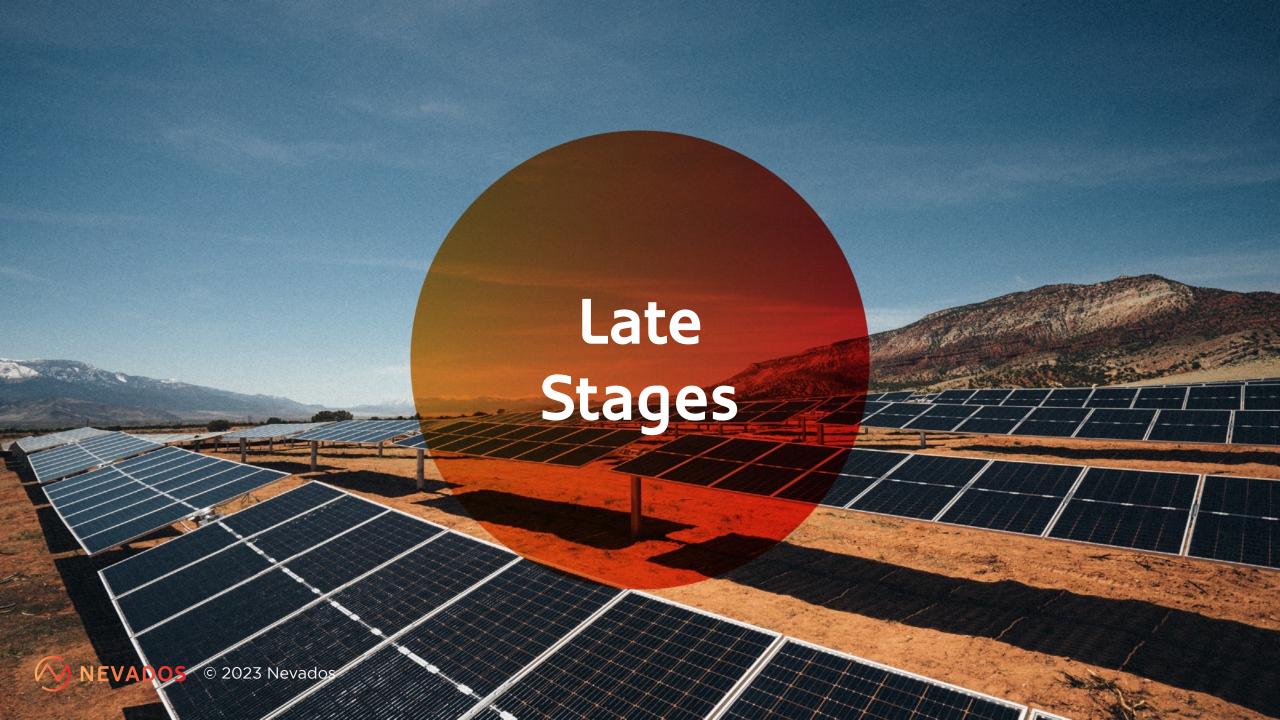




TRACKER QUOTATION

Nevados Quote Date Contact Contact 10/27/23. Valid for 14 Brittanie Jackson Phone Phone Location California 289.552.4128 Brittanie@nevados.solar 0

		escription				
			3 String	0		#N/A
		Interior	2 String	0		
			1 String	0		
	Material		Other	0	#N/A	
Structure	Material		3 String	0	#IV/A	#1V/A
		Exposed &	2 String	0		
		Exterior	1 String	0		
			Other	0		
	Logistics	DDP to Project S	ite; Incoterm 2020	0	#DIV/0!	0
	Total		#N/A	#N/A		
	Material	W6 Profile Summary on nex	0	#N/A	#N/A	
Foundations	Logistics	DDP to Project S	#DIV/0!	0		
	Total	#N/A	#N/A			
C	Material	#N/A	#N/A			
Structure +	Logistics	#DIV/0!	0			
Foundation	Total	#N/A	#N/A			
Additional	O&M Spai		#DIV/0!	#N/A		
Services	Structure I	Design	#DIV/0!	53,000		
	Base Warr	.0000	0			
Included Services	TRACE Ter	rain Aware Backtrac	king or True Trackin	g	.0000	0
Services	On-Site Su	upport (40 hrs) & Co	mmissioning		.0000	0
					#N/A	#N/A



Late Stage >30% with Engineering PO

- P.O. Signed
- Finalize Structural Reviews
 - Fully understand site conditions
 - Modules finalized
 - Leading edge requirement
 - Final Geotech and pull test reports supplied
- Finalize Foundations (as required)
- Final Layout from customer with civil details and grading plans



Point File Analysis (1-2

WeekSr vide Nevados with a point file based off proposed grading plans or expected site topography

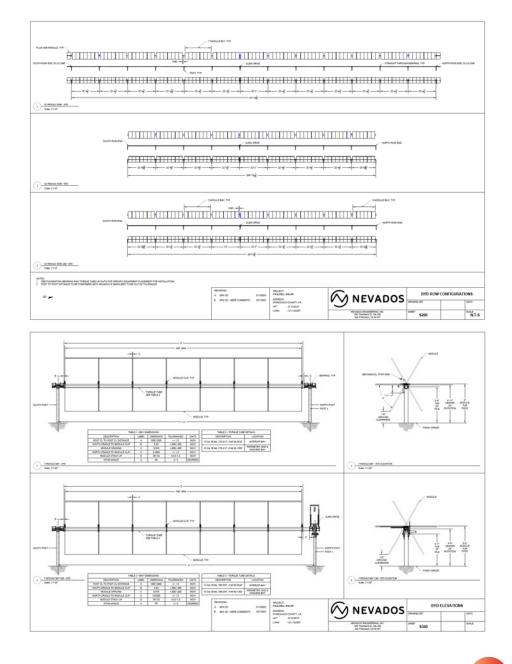
- This will be in the form of a CSV file that identifies Pile Locations with Easting, Northing, and Elevation
- The Point File will be used to allocate bearings to each pile based off the net angle change at the pile location with the following thresholds:
 - 4% (2.5 degrees)
 - 13% (7.5 degrees)
 - 27% (15 degrees)
- Torque Tubes will also be checked for minimum engagements and shifted if they are out of tolerance
- Potential to identify splicing, variable reveal heights, and spot grading
- B.O.M. finalized

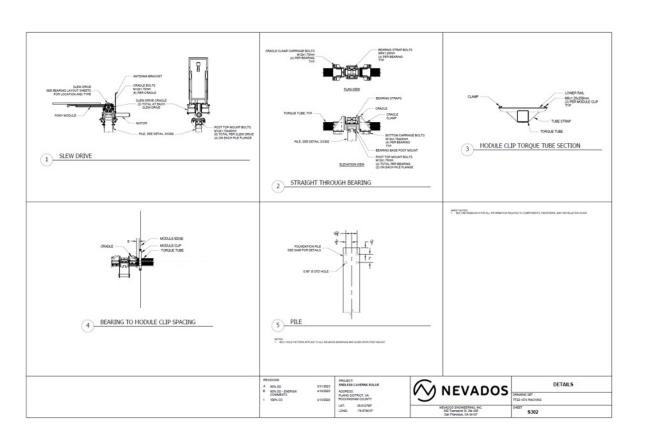


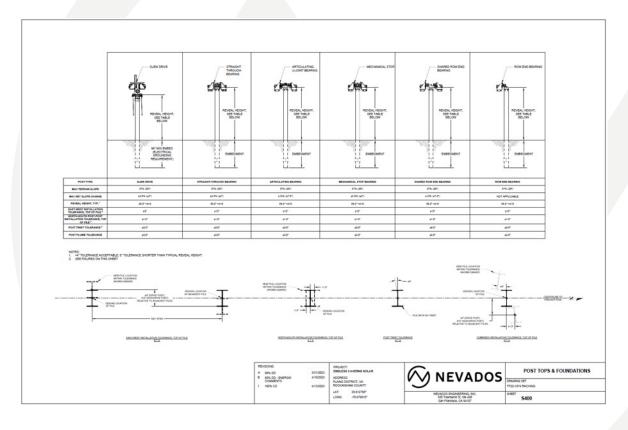
Reveal Height	z (top of pile)	Splice	bearing	exterior	block	tracker	z (bottom	у	x	Index
50.5	410.4733333		row end	FALSE	1	1	406.265	3858796	11666610	0
50.5	411.8193333		mechanical stop	FALSE	1	1	407.611	3858822	11666610	1
50.5	412.2073333		compact	FALSE	1	1	407.999	3858849	11666610	2
50.5	412.4733333		compact	FALSE	1	1	408.265	3858876	11666610	3
43.5	412.381		slew drive HE6	FALSE	1	1	408.756	3858903	11666610	4
50.5	413.6543333		compact	FALSE	1	1	409.446	3858929	11666610	5
50.5	414.2083333		compact	FALSE	1	1	410	3858956	11666610	6
50.5	414.3513333		compact	FALSE	1	1	410.143	3858983	11666610	7
50.5	414.8203333		mechanical stop	FALSE	1	1	410.612	3859010	11666610	8
50.5	415.1053333		shared row end	FALSE	1	1	410.897	3859037	11666610	9
50.5	415.4043333		mechanical stop	FALSE	1	1	411.196	3859064	11666610	10
50.5	415.7443333		compact	FALSE	1	1	411.536	3859091	11666610	11
50.5	416.1323333		compact	FALSE	1	1	411.924	3859118	11666610	12
43.5	415.806		slew drive HE6	FALSE	1	1	412.181	3859145	11666610	13
50.5	417.0383333		compact	FALSE	1	1	412.83	3859171	11666610	14
51.7	416.6723333	0.1	compact	FALSE	1	1	412.364	3859198	11666610	15
50.5	416.0093333		compact	TRUE	1	1	411.801	3859225	11666610	16
50.5	415.1213333		mechanical stop	TRUE	1	1	410.913	3859252	11666610	17
50.5	414.0793333		row end	TRUE	1	1	409.871	3859279	11666610	18
51.7	410.9383333	0.1	row end	FALSE	1	2	406.63	3858795	11666625	19
50.5	412.1073333		mechanical stop	FALSE	1	2	407.899	3858822	11666625	20
50.5	412.2133333		compact	FALSE	1	2	408.005	3858849	11666625	21
50.5	412.7733333		compact	FALSE	1	2	408.565	3858876	11666625	22
43.5	412.645		slew drive HE6	FALSE	1	2	409.02	3858903	11666625	23
50.5	413.8253333		compact	FALSE	1	2	409.617	3858929	11666625	24
50.5	414.2083333		compact	FALSE	1	2	410	3858956	11666625	25
50.5	414.7453333		compact	FALSE	1	2	410.537	3858983	11666625	26
50.5	415.2583333		mechanical stop	FALSE	1	2	411.05	3859010	11666625	27
50.5	415.5143333		shared row end	FALSE	1	2	411.306	3859037	11666625	28
50.5	415.8163333		mechanical stop	FALSE	1	2	411.608	3859064	11666625	29
50.5	416.1553333		compact	FALSE	1	2	411.947	3859091	11666625	30
50.5	416.5423333		compact	FALSE	1	2	412.334	3859118	11666625	31
43.5	416.42		slew drive HE6	FALSE	1	2	412.795	3859145	11666625	32
50.5	417.6143333		compact	FALSE	1	2	413.406	3859171	11666625	33
51.7	417.1713333	0.1	compact	FALSE	1	2	412.863	3859198	11666625	34
50.5	416.0493333		compact	TRUE	1	2	411.841	3859225	11666625	35
50.5	415.0383333		mechanical stop	TRUE	1	2	410.83	3859252	11666625	36
50.5	414.0203333		row end	TRUE	1	2	409.812	3859279	11666625	37
50.5	411.0033333		row end	FALSE	1	3	406.795	3858795	11666639	38
50.5	412.1913333		mechanical stop	FALSE	1	3	407.983	3858822	11666639	39

IFC Package (4-6 Weeks)

- IFC package to be kicked off after P.O. is signed
- Turnaround time of 4-6 weeks
- In 4-6 weeks, a draft will be provided to the customer for review and comments
- Edits from the draft review will be incorporated into the package
- After approval from customer, the package will be delivered to a P.E. for stamping
- Typical 2-week turnaround time for stamped package and calculation
- Foundation package will also require P.E. stamping and calculations
- P.E. will provide general notes, materials, and codes in the stamped package

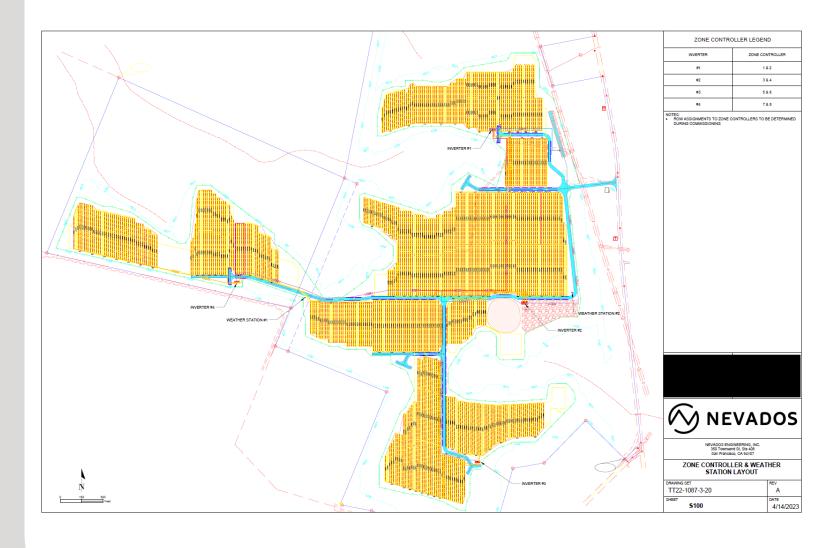






Zone Controller & Weather Station Layout

- Require iteration with customer to place weather stations in buildable areas
- Potential Impact to civil design
- Zone Controllers will be designed at inverted pads with 1-2 per pad



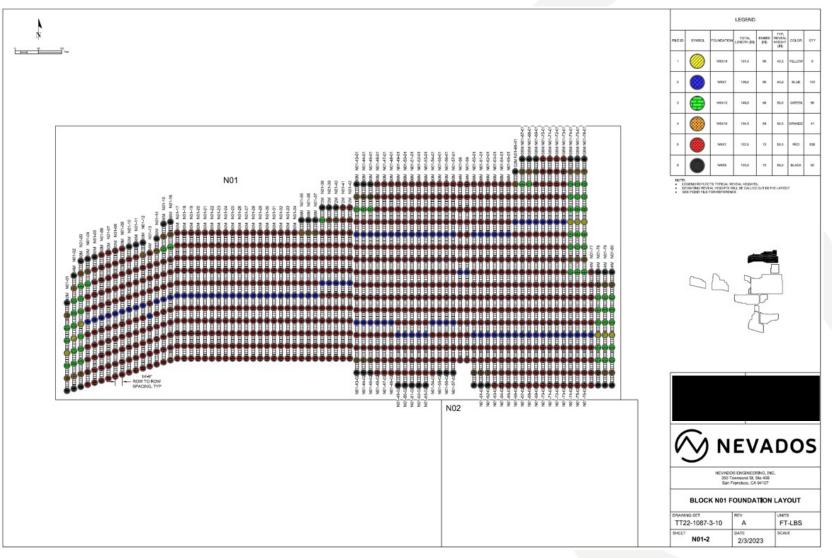


Construction and Commissioning

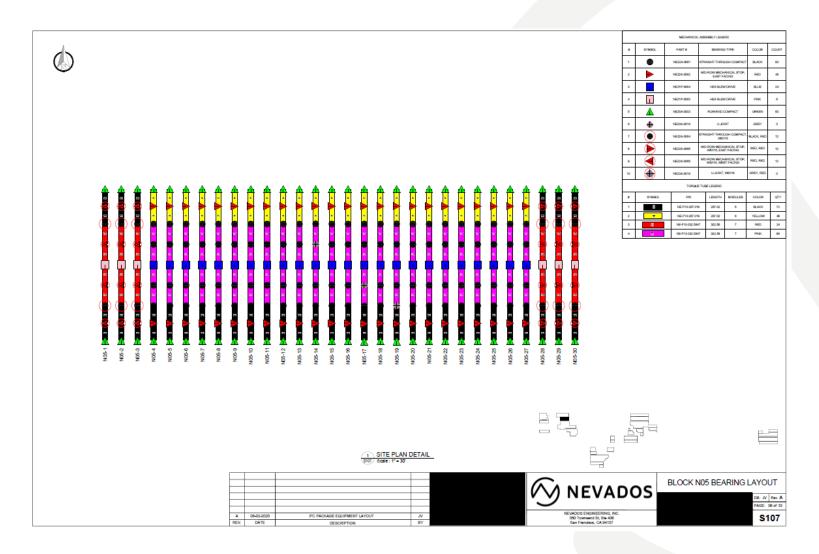


- Provide equipment 30 days prior to first delivery or earlier
- Customer to provide clear timelines with milestones
 - Pile install start and finish
 - Equipment install start and finish
 - Commissioning start and finish
- Align Nevados controls with on-site SCADA and network teams
- Align delivery schedules and crews involved with receiving
- Provide equipment staging plan
- Schedule virtual product training with relevant parties involved in construction
- Schedule golden row training after virtual product training
- Schedule Nevados support for commissioning if required

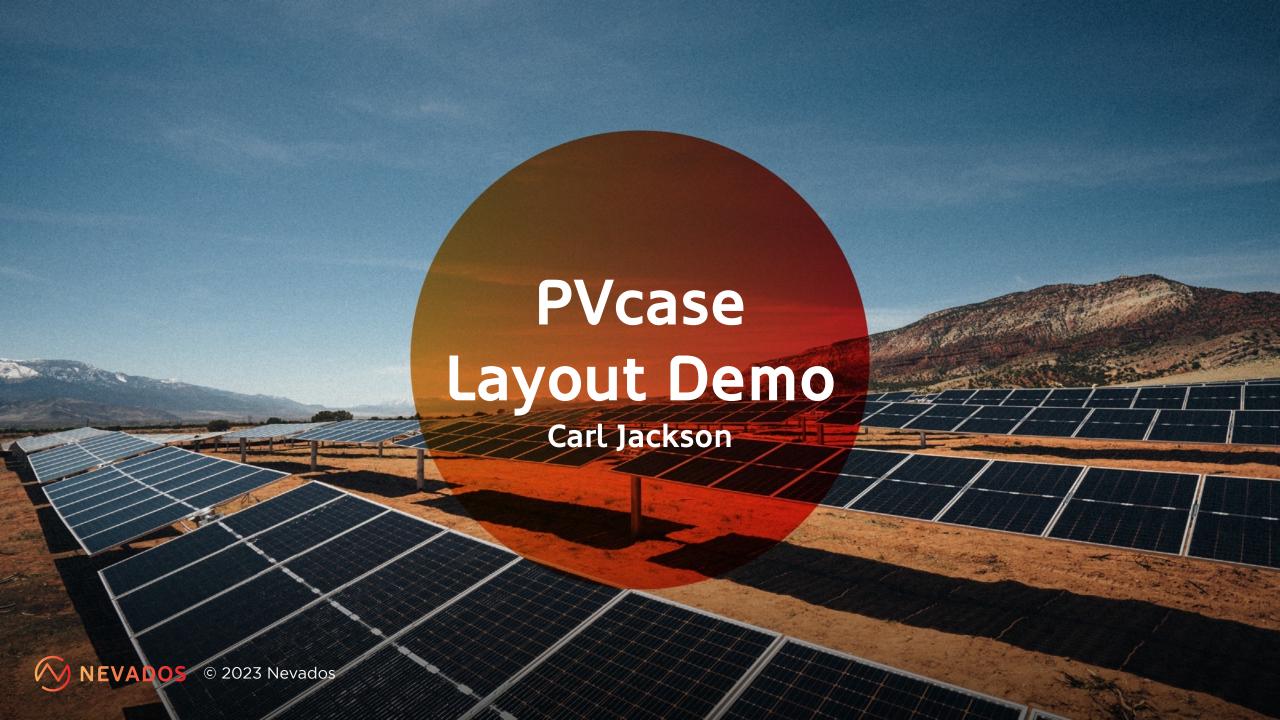
Foundation Layout



Mechanical Assembly Layout







PVcase BENEFITS:



Allows more accurate analysis of topography at preliminary layout stage

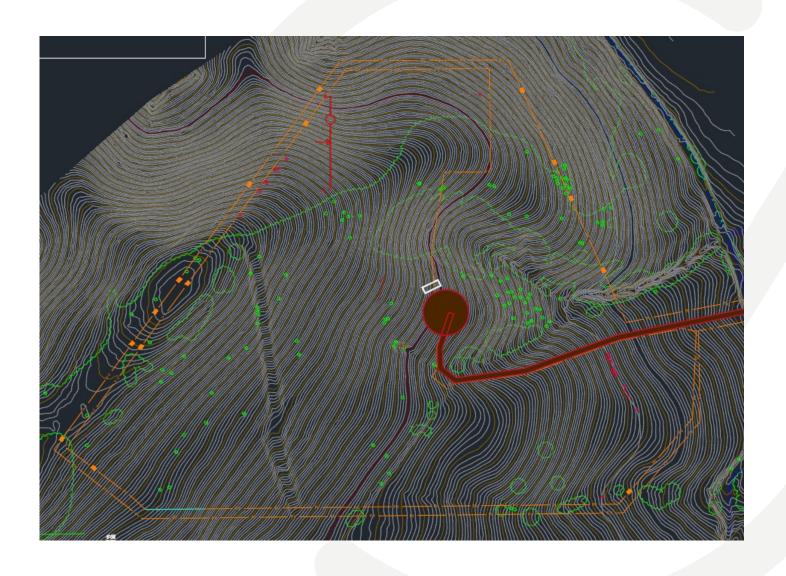


Allows more accurate preliminary BOM's, and allows easy communication with customers/ EPC's who use PVcase



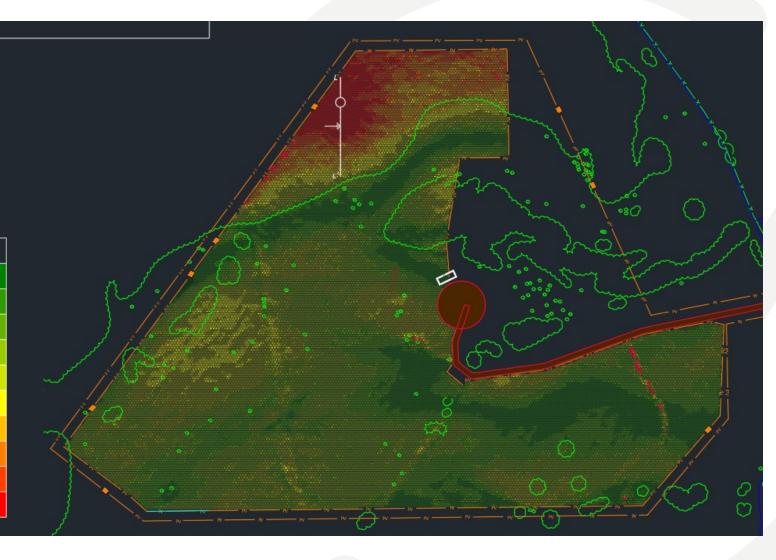
Allows for quick generation of challenging layouts at preliminary design stages and allows for easy adjustments/iterations in azimuth and capacity

Input site plans with topography lines is used to generate a surface mesh



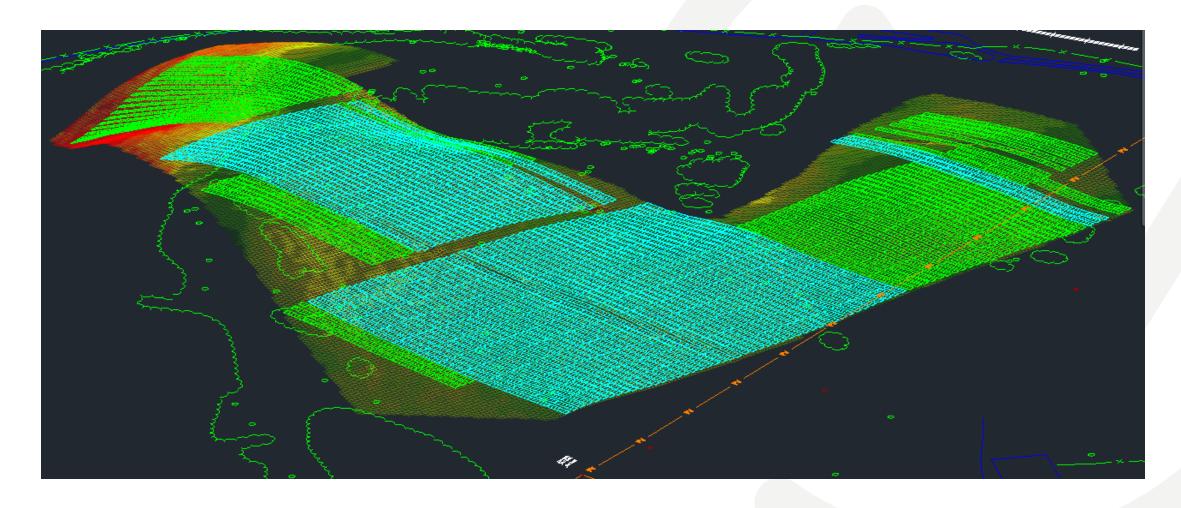
Surface mesh and distribution table

Angle min., %	Angle max., %	Distribution, %	Color
0.00	0.00	0.03	
0.00	4.62	14.30	
4.62	9.25	22.01	
9.25	13.88	33.15	
13.88	18.50	15.37	
18.50	23.12	4.67	
23.12	27.75	2.44	
27.75	32.38	3.57	
32.38	37.00	2.02	
37.00	142.81	2.44	

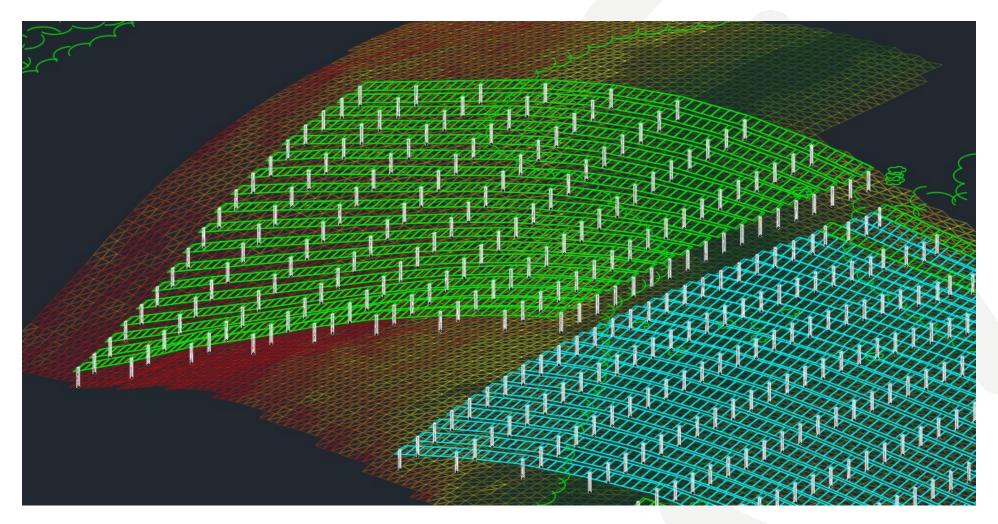




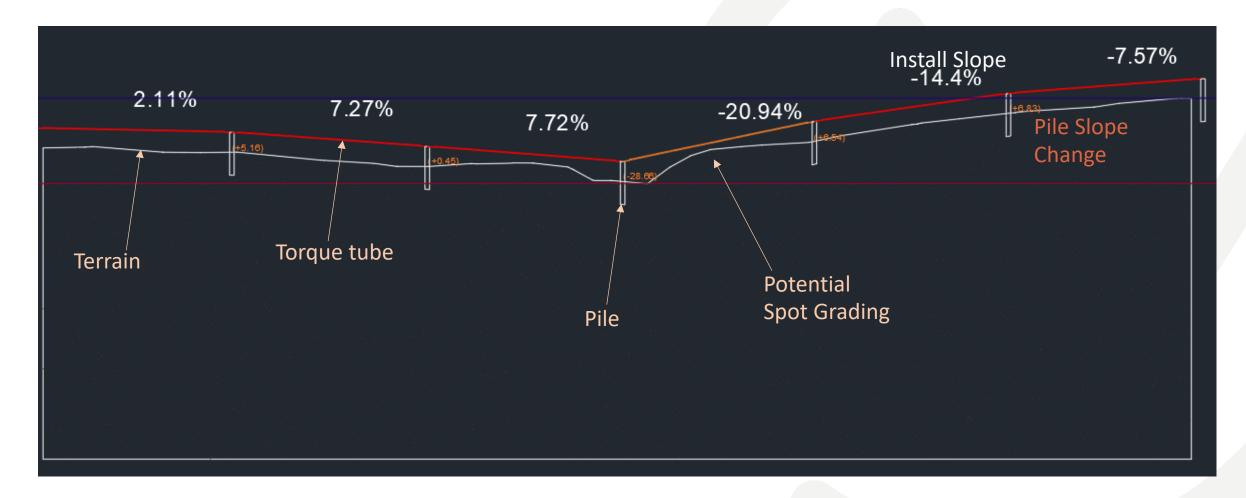
Layout Generation on top of surface



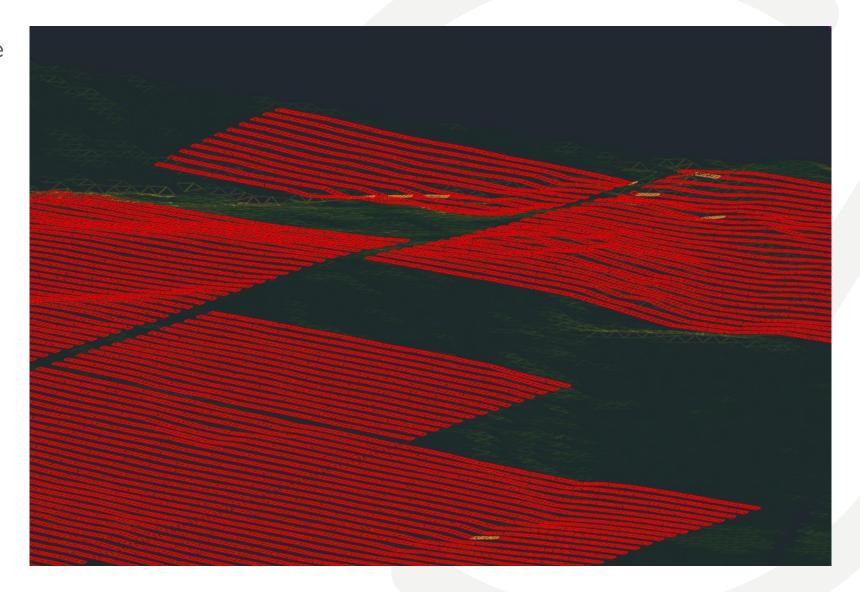
Piles rendered



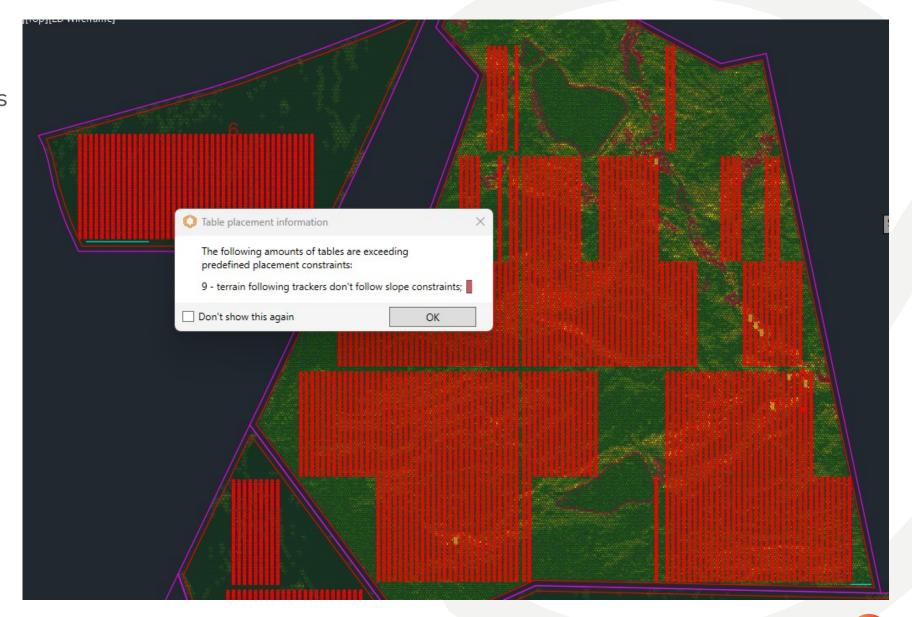
Cross Section, slope at point and bearing angle at point



Indicative frames showing angle greater than set point



These show bays that need double articulating bearings



Demo







Highlights

- → 30x faster designs
- → 11% increase in capacity
- → 9% more precise cable lengths
- → 13% increase in energy production
- → Operating in over 60 countries

